## **H4.1 Moment-Curvature** (M-φ) **Diagram**

The stress-strain curves of **M25** grade *unconfined* concrete and the associated *confined* concrete are shown in **Figure H4.1(a)**, and that of **Fe500** grade reinforcing steel in **Figure H4.1(b)**. The values of salient points of the stress-strain curves are given in **Table H4.1**. The expressions of stress-strain curves of concrete follows *parabolic-linear* path (Eq.(H4.1)), and of reinforcing steel follows *elasto-plastic* path (Eq.(H4.2)).

Using these material constitutive laws, write a computer program to obtain the **Moment-Curvature** (M- $\phi$ ) **Diagrams** of the RC pier section shown in **Figure H4.2**. The following cases need to be studied:

- (a) The concrete in the entire cross-section is unconfined, and
  - (i)  $P_D$ =2,000 kN, (ii)  $P_D$ =4,000 kN, (iii)  $P_D$ =8,000 kN, (iv)  $P_D$ =12,000 kN, and (v)  $P_D$ =16,000kN; and
- (b) The concrete in the cover region of the cross-section is *unconfined*, and in the core region is *confined*, and
  - (i)  $P_D$ =2,000 kN, (ii)  $P_D$ =4,000 kN, (iii)  $P_D$ =8,000 kN, (iv)  $P_D$ =12,000 kN, and (v)  $P_D$ =16,000kN; and

Draw the M-φ Curves of the said cases on a single graph.

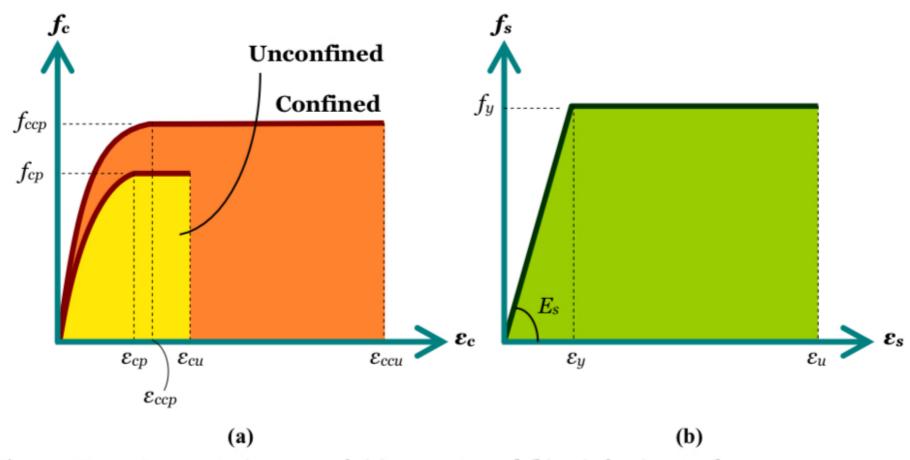


Figure H4.1: Stress-strain curve of: (a) concrete and (b) reinforcing steel

Table H4.1: Values of salient points of stress-strain curves

Concrete	f <sub>c</sub> at peak (MPa)	$arepsilon_{ m c}$ at peak $f_{ m c}$	$arepsilon_{ m c}$ at ultimate
Unconfined	25.0	0.0020	0.0035
Confined	32.5	0.0025	0.0100
Steel	fy (MPa)	$oldsymbol{arepsilon}_y$	$\boldsymbol{\varepsilon}_{u}$
Longitudinal	500	0.0025	0.1200

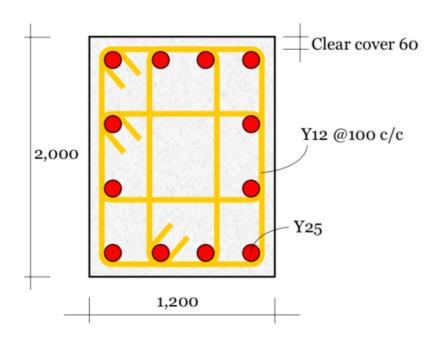
Unconfined concrete: 
$$f_{c} = \begin{cases} f_{cp} \left[ 2 \left( \frac{\mathcal{E}_{c}}{\mathcal{E}_{cp}} \right) - \left( \frac{\mathcal{E}_{c}}{\mathcal{E}_{cp}} \right)^{2} \right] &: 0 \leq \mathcal{E}_{c} \leq \mathcal{E}_{cp} \\ f_{cp} &: \mathcal{E}_{cp} < \mathcal{E}_{c} \leq \mathcal{E}_{cu} \end{cases}$$

$$(H4.1(a))$$

Confined concrete: 
$$f_{c} = \begin{cases} f_{ccp} \left[ 2 \left( \frac{\varepsilon_{c}}{\varepsilon_{ccp}} \right) - \left( \frac{\varepsilon_{c}}{\varepsilon_{ccp}} \right)^{2} \right] &: 0 \leq \varepsilon_{c} \leq \varepsilon_{ccp} \\ f_{ccp} &: \varepsilon_{ccp} < \varepsilon_{c} \leq \varepsilon_{ccu} \end{cases}$$

$$(H4.1(b))$$

Reinforcing steel: 
$$f_s = \begin{cases} E_s \varepsilon_s &: 0 \le \varepsilon_s \le \varepsilon_y \\ \\ f_y &: \varepsilon_y \le \varepsilon_s \le \varepsilon_u \end{cases}$$
 (H4.2)



**Figure H4.2:** Cross-section geometry of RC pier (all dimensions are in mm)

20 Marks

2

## H4.2 Axial Force – Bending Moment (P-M) Interaction Diagram

Write a computer program to draw the **Axial Force** – **Bending Moment** (P-M) **Interaction Diagram** for *case* (a) and *case* (b) given in **H4.1**. Mark the *axial force* (P) and *bending moment* (M) values obtained from the *moment-curvature analysis* of **H4.1** in the corresponding P-M interaction diagram. **Comment** on the results obtained.